

## SYMBOLS

(only the most important symbols for presentation and application of the method)

(the symbols in Courier New are those visualized in graph mode)

### Latin

' , "	Principal axes of plane state of stress
$A$	Constant in $S-N$ line equation; constant for $\sigma'$
$A$	Side of square in graph mode
$a$	Mathematical expression in the role of coefficient of elliptic equation
$a$	Amplitude index
$As$	Addend to $s(t)$ ; $s_m$
$B$	Constant for $\sigma'$
$b$	Mathematical expression in the role of coefficient of elliptic equation
$C$	Static center of a variant trajectory (its coordinates are $\sigma_{x,m}$ , $\sigma_{y,m}$ and $\tau_{xy,m}$ )
$c$	$-1/s^2$ in the role of coefficient of elliptic equation
Code 1:	$\sigma_x(t)$ , $\sigma_y(t)$ and $\tau_{xy}(t)$ are entered; $X-Y \equiv \sigma'-\sigma''$ ; Nrct=3
2:	$\sigma_x(t) \equiv \sigma'(t)$ and $\sigma_y(t) \equiv \sigma''(t)$ are entered; $X-Y \equiv \sigma'-\sigma''$ ; Nrct=2
3:	$\sigma(t) \equiv \sigma_x(t)$ and $\tau(t) \equiv \tau_{xy}(t)$ are entered; $X-Y \equiv \sigma'-\sigma''$ ; Nrct=3
4:	$\sigma(t) \equiv \sigma_x(t)$ and $\tau(t) \equiv \tau_{xy}(t)$ are entered to appear along $\xi$ and $\eta$ ; Nrct=2
5:	$\varepsilon_x(t)$ , $\varepsilon_y(t)$ and $\gamma_{xy}(t)$ are entered; $X-Y \equiv \varepsilon'-\varepsilon''$ ; Nrct=3
6:	$\varepsilon_x(t)$ , $\varepsilon_y(t)$ and $\varepsilon_b(t)$ are entered from $x$ - $y$ - $b$ rosette; $X-Y \equiv \varepsilon'-\varepsilon''$ ; Nrct=3
$D$	Fatigue Damage; $D(s) = 1/[i^* N(s)]$ is primitive function to $R(s)$
$D$	Symbol for $D_\Sigma$ in graph mode
$d$	Differential (that is numerically substituted by $\Delta$ )
$d_c$	Ratio of damages: $d_c = D_{\Sigma,c,T}/D_{\Sigma,T}$
$dD$	Damage differential; $dD_r$ is per $ds_r$ ; $dD_c$ is per $ds_c$ ; $dD_\tau$ is per $d\tau$
$d_r$	Ratio of damages: $d_r = D_{\Sigma,r,T}/D_{\Sigma,T}$
$ds$	Loading differential
$Ds$	Devisor of $s(t)$
$ds_c$	Circumferential component of $ds$ and $ds_{xy}$
$ds_r$	Radial component of $ds$ and $ds_{xy}$
$ds_{xy}$	Component of $ds$ in $X$ - $Y$ plane
$D_T$	Damage per a cycle within $T$

$D_{\Sigma}$	Cumulative (current) damage.
$D_{\Sigma,cr}$	Critical accumulated damage ( $D_{\Sigma,cr} = 1$ in this thesis)
$D_{\Sigma,c,T}$	Damage accumulated in $T$ as a sum of differentials $\Delta D_c$
$D_{\Sigma,r,T}$	Damage accumulated in $T$ as a sum of differentials $\Delta D_r$
$D_{\Sigma,T}$	Damage totally accumulated in $T$ as a sum of differentials $\Delta D$
$D_{\Sigma,\tau,T}$	Damage accumulated in $T$ as a sum of differentials $\Delta D_{\tau}$
$d\tau$	Component of $ds$ perpendicular to the $\sigma'-\sigma''$ plane.
$d_{\tau}$	Ratio of damages: $d_{\tau} = D_{\Sigma,\tau,T}/D_{\Sigma,T}$ .
$E$	Young modulus
$f$	Ratio $f = R/R_r$ in case a single $R$ -intensity is used
$f_c$	Factor of (sensitivity of the material to) loading non-proportionality (associated with immovability of the principal axes): $f_c = R_c/R_r$
$f_{\tau}$	Factor of (sensitivity of the material to) loading non-proportionality (associated with rotation of the principal axes): $f_{\tau} = R_{\tau}/R_r$
$i$	Counter of the input prototypes, $i = 1, 2, \dots, n$ ; counter of the addends of sums
$\dot{i}$	Counter of the trajectory elements in graph mode; counter for other purposes
$i^*, \dot{i}^*$	Divisor for static (mean) stress, respectively for loading asymmetry
$j$	Number of trajectory elements to be displayed in a group; counter for other purposes
$k, k$	Ratio $k(t) = Y(t)/X(t)$ ; $k(t)$ is mostly $\sigma'(t)/\sigma'(t)$ ; $k = \text{const}$ under one-component or proportional loading and for an input $R$ -prototype
$k_i$	$k$ for $i^{\text{th}}$ input $R$ -prototype (one of its parameters, see also $\sigma'_{\max,i}$ )
$L$	No-damage area (with $R = 0$ ) in the $X$ - $Y$ plane; the curved limiting line surrounding that area; $L$ is particularly $L_r$ (or $L_l$ ) for $R_r = 0$ , $L_c$ for $R_c = 0$ and $L_{\tau}$ for $R_{\tau} = 0$ ; the $L$ line is a limiting $l_N$ line of equal life $N \equiv N_{\text{ex}}$
$l$	Index of limit (or of fatigue failure locus, etc.)
$l_{\text{equ,m}}$	Line of equal equivalent mean (static) stress $\sigma_{\text{equ,m}}$
$L_{\min}$	Absolute smallest no-damage area.
$l_N$	Line of equal life $N$ (from $R_r$ -prototypes) under cyclic proportional or one-component loadings (cyclic $r$ -loadings)
$L_N$	Life name in graph mode
$m, m$	(Indicator of) slope of an $S$ - $N$ line
$m$	Mean (static) stress index
$\max$	Index of maximum of stress cycle or maximum in a oscillogram

maxX	Fixes the right side of the square in graph mode
$m_i$	$m$ of $i^{\text{th}}$ input $R$ -prototype (one of its parameters, see also $\sigma'_{\max,i}$ )
min	Index of minimum of stress cycle or minimum in a oscillogram
minX	Fixes the left side of the square in graph mode
minY	Fixes the lower side of the square in graph mode
$m_l, Ml$	Multiplier of life
Ms	Multiplier of $s(t)$
$N$	Life as a number of repetitions of $T$ to fatigue failure: $N = 1/D_{\Sigma,T}$ ; number of cycles to failure, function $N(s) \equiv N(s_{\max})$ ; abscissa of a point of an $S-N$ line
$n, n$	Number of input prototypes, $2 \leq n \leq 9$ ; number of input ordinates of $s(t)$ to be processed by <i>Integral</i> program; fatigue safety factor
n1	Serial number of first series to be processed by <i>EllipseS</i> program
n2	Serial number of last series to be processed by <i>EllipseS</i> program
$N_c$	Number of cycles (see also $N_{\text{ex}}$ ) for forming the limiting line (the no-damage area) $L_c$
$N_{\text{cmp}}$	Computed life
$N_{\text{ex}}$	Extrapolated number of cycles; it may be $N_{\text{ex},r}$ , $N_{\text{ex},c} \equiv N_c$ and $N_{\text{ex},\tau} \equiv N_{\tau}$ ; $N_{\text{ex},r}$ may be $N_r$ in smooth mode or $N_l$ in breaking mode
$N_{\text{ex}}$	See $N_{\text{ex}}$
$N_{\text{exp}}$	Experimental life
$N_i$	Abscissa of through-point of $i^{\text{th}}$ input $R$ -prototype (see also $\sigma'_{\max,i}$ )
$n_i, Ni$	Number for interpolation; in <i>EllipseT</i> , $n_i$ can be 1, 2, 3, 4, 6, 8, 12, 24 (24 is divisible by these values); in <i>EllipseS</i> , $n_i$ can be any integer greater than 0; $n_i = 1$ means no interpolation
$N_l, Nl$	Number of cycles at the break of $S-N$ line; serves for forming the limiting line (the no-damage area) $L_l$ (in breaking mode)
$N_r$	Number of cycles (see also $N_{\text{ex}}$ ) for forming the limiting line (the no-damage area) $L_r$ (in smooth mode)
$N_{\text{rct}}$	Number of $R$ functions: 3, the $R$ functions are $R_r$ , $R_c$ and $R_{\tau}$ ; or 2, the $R$ functions are $R_r$ and $R_c$ ; see also Code
$n_v, Nv$	Number of values in a series for interpolation
$N_{\tau}$	Number of cycles (see also $N_{\text{ex}}$ ) for forming the limiting line (the no-damage area) $L_{\tau}$
$p_i$	Relative statistical frequency of within a $\Delta s_i$ interval
$p_{ij}$	Relative statistical frequency of appearing $\Delta s$ elements within an (i,j) cell
$q_k$	Quotient (ratio) $\sigma'_m/\sigma'_{\text{equ},m}$ at given $k$ at $l_{\text{ekB},m}$ line; $q_k = \sigma'_k/\sigma'_{k=0}$ at $l_N$ line

$R$	Damage intensity, $R$ function of $\sigma'$ and $\sigma''$ (or of $\varepsilon'$ and $\varepsilon''$ , etc.); $R(s) = dD(s)/ds$ is derivative function to $D(s)$ ; in particular, $R$ is $R_r$ , $R_c$ , $R_\tau$
$R$	Stress ratio: $R = s_{\max}/s_{\min}$
$R_c$	Damage intensity at $ds_c$
$R_m$	(Ultimate) static strength measure ( $\sigma_U$ )
$R_{p0.2}$	Yield strength measure ( $\sigma_Y$ )
$R_r$	Damage intensity at $ds_r$
$R_\tau$	Damage intensity at $d\tau$
$S, s$	Stress; sum of $\Delta s$ elements ( $ds$ differentials), length of ( $S$ ) trajectory
$s, s$	Stress; distance from the coordinate origin to the running point of a trajectory, argument of $R(s)$ and $D(s)$
$(S)$	Invariant trajectory consisting of $\Delta s$ elements ( $ds$ differentials).
$S_c$	Sum of $\Delta s_c$ elements ( $ds_c$ differentials), length of ( $S_c$ ) trajectory
$(S_c)$	Trajectory consisting of $\Delta s_c$ differentials ( $ds_c$ differentials)
$s_l, s_l$	Fatigue limit ( $s_l \equiv s_{\max, l}$ )
$s_r, s_r$	Limit to which an $R_r$ prototype is extrapolated in smooth mode
$S_r$	Sum of $\Delta s_r$ elements ( $ds_r$ differentials), length of ( $S_r$ ) trajectory
$(S_r)$	Trajectory consisting of $\Delta s_r$ elements ( $ds_r$ differentials)
$S_{xy}$	Sum of $\Delta s_{xy}$ elements ( $ds_{xy}$ differentials), length of ( $S_{xy}$ ) trajectory
$(S_{xy})$	Trajectory in $X$ - $Y$ plane (that is mostly $\sigma'$ - $\sigma''$ plane) consisting of $\Delta s_{xy}$ elements ( $ds_{xy}$ differentials)
$S_\tau$	Sum of $\Delta \tau$ elements ( $d\tau$ differentials), length of ( $S_\tau$ ) trajectory
$(S_\tau)$	Trajectory consisting of $\Delta \tau$ elements ( $d\tau$ differentials)
$T$	Time interval representative for the loading; period, cycle
$t$	Time
$t_c$	Trajectory ratio $S_c/S$
$t_r$	Trajectory ratio $S_r/S$
$t_\tau$	Trajectory ratio $S_\tau/S$
$v_i$	Axis of an ellipse giving its arc for composition of a line of equal life by involving input prototypes with indexes $i$ and $i+1$
$x, y$	Variant (non-principal) axes of plane state of stress
$X, Y$	Common symbols for the axes of the coordinate plane of trajectory ( $S_{xy}$ ); mostly, $X \equiv \sigma'$ , $Y \equiv \sigma''$ ; see also Code; coordinates of current point of ( $S_{xy}$ ) trajectory

$x, y$  See  $X, Y$

$X_0, Y_0$  Coordinates of previous point of  $(S_{xy})$  trajectory

$x_0, y_0$  See  $X_0, Y_0$

### Greek

$\alpha$  Angle measured from  $x$  at which an infinitesimal cuboid is orientated

$\alpha_0$  Angle of orientation of the principal cuboid;  $\alpha_0 = \alpha$  if  $\alpha$  is within the interval  $(-45^0, +45^0)$  and  $\alpha_0 = \alpha'$  if  $\alpha'$  is within the interval  $(+45^0, -45^0)$

$\alpha'$  The angle at which the principal axis ' always is

$\alpha''$  The angle at which the principal axis '' always is

$\gamma$  Shear strain

$\gamma_{xy}^*$   $\gamma_{xy}^* = \gamma_{xy}/2$

$\Delta$  Finite difference substituting d differential; short straight-line segment (element)

$\delta$  Initial phase angle; phase-shift angle; out-of-phase angle

$\Delta\tau$  Component of  $\Delta s$  perpendicular to the  $\sigma'$ - $\sigma''$  plane

$\varepsilon$  Normal strain

$\varepsilon', \varepsilon''$  Principal strains

$\eta$  The bisector of the quadrants I and III of equal algebraic signs; coordinate (along the  $\eta$  axis) of the invariant (principal) point  $(\sigma', \sigma'')$ :  $\eta = (\sigma' + \sigma'')/\sqrt{2}$

$\nu$  Poisson ratio

$\xi$  The bisector of the quadrants II and IV of opposite algebraic signs; coordinate (along the  $\xi$  axis) of the invariant (principal) point  $(\sigma', \sigma'')$ :  $\xi = (\sigma' - \sigma'')/\sqrt{2}$

$\xi^*$   $\xi^* = (\sigma' - \sigma'')/2$  or  $\xi^* = (\varepsilon' - \varepsilon'')/2$

$\xi_v^*$   $\xi_v^* = (\sigma_x - \sigma_y)/2$  or  $\xi_v^* = (\varepsilon_x - \varepsilon_y)/2$

$\rho$  Two-dimensional or one-dimensional density of an  $(S)$  trajectory; two-dimensional density (spectrum) of joint (mutual) distribution of the instantaneous (current) values of  $X(t)$  and  $Y(t)$ ; one-dimensional density (spectrum) of distribution of the instantaneous (current) values of  $s(t)$

$\rho_{ij}$   $\rho_{ij} = p_{ij}/(\Delta X \cdot \Delta Y)$  is discrete two-dimensional density

$\sigma$  Normal stress;  $\sigma_x, \sigma_y$  and  $\tau_{xy}$  are the three stresses on a variant cuboid, and are the coordinates of the running (current) point of the variant trajectory in the  $\sigma_x$ - $\sigma_y$ - $\tau_{xy}$  coordinate space

$\sigma_{-1}$  Fatigue limit of reversed stress cycle of uniaxial state of stress

- $\sigma', \sigma''$  Principal stresses; coordinates of running (current) point of ( $S_{xy}$ ) trajectory
- $\sigma'_{\max, i}$  Ordinate of through-point of  $i^{\text{th}}$  input  $R$ -prototype ( $\sigma'_{\max}, N, m, k, \psi$ ) <sub>$i$</sub>   $\equiv (\sigma'_{\max, i}, N_i, m_i, k_i, \psi_i)$  against the abscissa  $N_i$ , and the prototype is an  $S$ - $N$  line having the equation
- $$\sigma'_{\max}{}^{m_i} N = \sigma'_{\max, i}{}^{m_i} N_i$$
- $\sigma'_p, \sigma''_p$  Coordinates of previous (preceding, old) point of ( $S_{xy}$ ) trajectory
- $\sigma_{\text{equ}}$  Equivalent stress
- $\sigma_{\text{equ}, m}$  Equivalent static (mean) stress (equivalent to  $\sigma_{x, m}, \sigma_{y, m}$  and  $\tau_{xy, m}$ )
- $\sigma_U$  (Limit of) ultimate (static) strength ( $R_m$ )
- $\sigma_Y$  (Limit of) yield (static) strength ( $R_{p0.2}$ )
- $\tau$  Shear stress (see also  $\sigma$ )
- $\tau_1$  Fatigue limit of reversed stress cycle of pure shear
- $\tau_U$  (Limit of) ultimate (static) pure shear strength
- $\tau_Y$  (Limit of) yield (static) pure shear strength
- $\psi_i$  Angle of deviation of  $v_i$  from  $\eta$ ,  $-45^\circ < \psi_i < 45^\circ$ , one of the parameters of  $i^{\text{th}}$  input  $R$ -prototype (see also  $\sigma'_{\max, i}$ )
- $\Omega$  The least possible area of the plane  $X$ - $Y$  ( $\sigma'$ - $\sigma''$  etc.) from which a concrete invariant ( $S$ ) trajectory does not go out
- $\omega$  Angular frequency; angular velocity